

ADA 036609 NUWC-TN-126 **NAVAL UNDERSEA WARFARE CENTER** JUNE 1968 COPY AVAILABLE TO ODG DOES NOT PERMIT FULLY LEGIBLE PRODUCTION Technical + M CALCULATION OF ABSORPTION COEFFICIENT USING AVERAGE TEMPERATURE AND PRESSURE. by L. P. Berger & H. R. Hall San Diego, California SUBPROJECT NO. ZR0110101 TASK NO. 0401

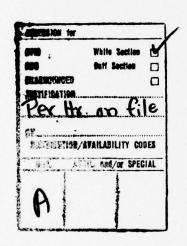
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This technical note describes a calculation procedure for a prediction model presently in use at the Naval Undersea Warfare Center,

San Diego Division. This note is not to be considered as an official

NUWC report. Its purpose is to document the existing model to the extent required by Navy project offices for whom predictions have been made.

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INTRODUCTION

This note describes the investigation of an expression to be used in bottom bounce propagation models presently in use at NUWC Code D556.

Recently an expression was developed to predict the acoustic absorption coefficient of seawater from the frequency, temperature, pressure and salinity. This expression was developed from a combination of existing equations in order to provide a single prediction expression valid under all operating conditions.

In the past many methods of calculating the absorption coefficient have been used. These methods include the use of the surface temperature and 50°F in empirical expressions. This paper shows that it is necessary for the sake of accuracy to use the temperature averaged over the path of the propagating ray and to include the pressure term.

## SUMMARY AND CONCLUSIONS:

The acoustic absorption coefficient ( $\alpha$ ) of sea water for any particular point is a function of the temperature (T) and the pressure (P) at that point, as well as the frequency (f) and the relaxation frequency (f<sub>T</sub>). Several methods of averaging  $\alpha$  over temperature-depth profiles were compared for accuracy and ease of computation. The difference between the absorption calculated using depth-averaged temperature and that using the surface temperature or the bottom temperature is shown in figure 3. The temperature can be averaged in Procedure RAYTRACE\* by using the existing values of depth and time increment with five new ETRAN statements.

<sup>\*</sup>Procedure RAYTRACE is a computer program which computes raypath parameters using Snell's Law and a velocity profile comprised of constant gradient sections.

The absorption loss results compare favorably with those calculated using each temperature and averaging the results.

Errors due to deletion of the pressure term in  $\alpha$  calculations can be significant at large depths (>2x10 ft) and higher frequencies (>3kHz). Neglecting the increase in density, the static pressure is a linear function of depth and can be averaged in Procedure RAYTRACE with the addition of three new statements.

## PROCEDURE:

The expression for the acoustic absorption of sea water 1 is

$$\alpha = \frac{1.776f^{1.5}}{32.768+f^3} + \left(\frac{1-6.54 \times 10^{-4} P}{1+32.768/f^3}\right) \cdot \left(\frac{.6505 f_T^2 f^2}{f^2 + f_T^2} + \frac{.02685 f^2}{f_T}\right) dB/kyd$$

where  $\,f_{\tau}^{}\,$  is calculated as below.

$$f_{T} = 21.9 \times 10^{(6T+118)/(T+213)} \text{ kHz}$$

The average temperature is calculated from

$$T = \frac{1}{t} \sum_{k=1}^{n} T_k t_k$$

where  $T_k$  is the temperature during the time period  $t_k$  and t is the total time during the averaging process. The average relaxation frequency was calculated in the same manner.

The coefficient of absorption was calculated separately using the average temperature, the average relaxation frequency, the surface temperature, and the bottom temperature. The coefficient was also determined for each break in the temperature-depth profile and averaged to provide a physically accurate value for comparison.

The above calculations were made for several temperature-depth profiles derived from bathythermograph and Nansen cast data (figure 1) assuming that the time spent at each temperature is proportional to the depth interval of that temperature. Calculations were then made for a general profile (figure 2) using time intervals calculated by Procedure RAYTRACE, which gives the actual time spent by the ray in each depth interval.

The values of  $\alpha$  as a function of frequency resulting from the application of these averaging techniques to the general profile are shown in figure 3. It is seen that the value determined through temperature averaging is nearly equal to the corresponding value determined by averaging the coefficients for each temperature along the profile.

The differences between the absorption loss at a range of 50 kyd determined by the surface and the bottom temperatures are shown in figure 4. Results are shown for several operating frequencies. Figures 5, 6 and 7 show a comparison of  $\alpha$  determined using the surface temperature, the bottom temperature, and the average temperature for several varied temperature profiles at a reference distance of one kiloyard.

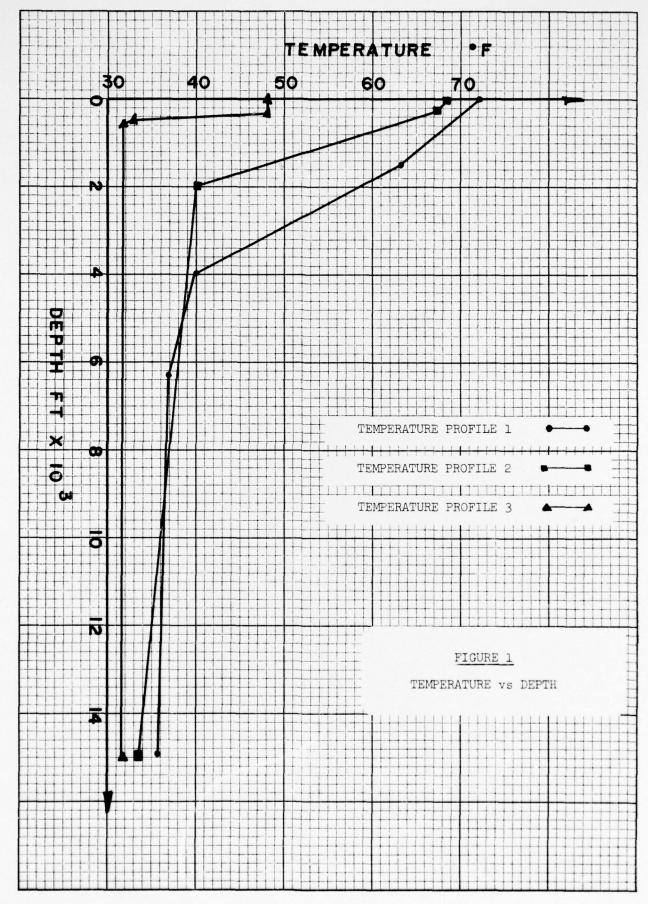
The variations in the absorption loss caused by pressure are shown in figure 8 for several frequencies and depths.

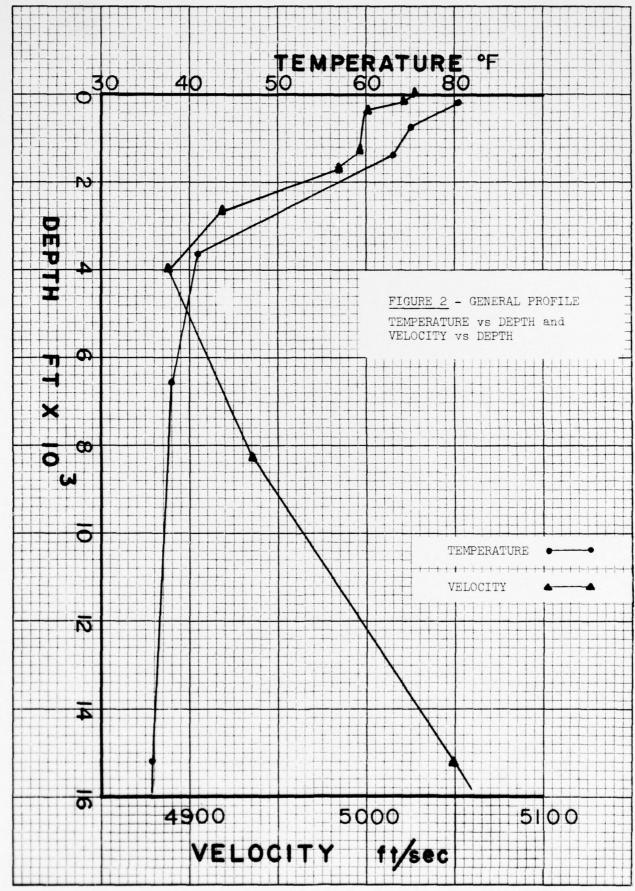
The temperature and pressure averaging procedures described in this note are being implemented in a modified Procedure RAYTRACE<sup>4</sup> which will be documented in the near future. A direct application of this technique is in the Bottom Bounce Propagation Mode. Adaptations are also being considered for the Convergence Zone Mode.

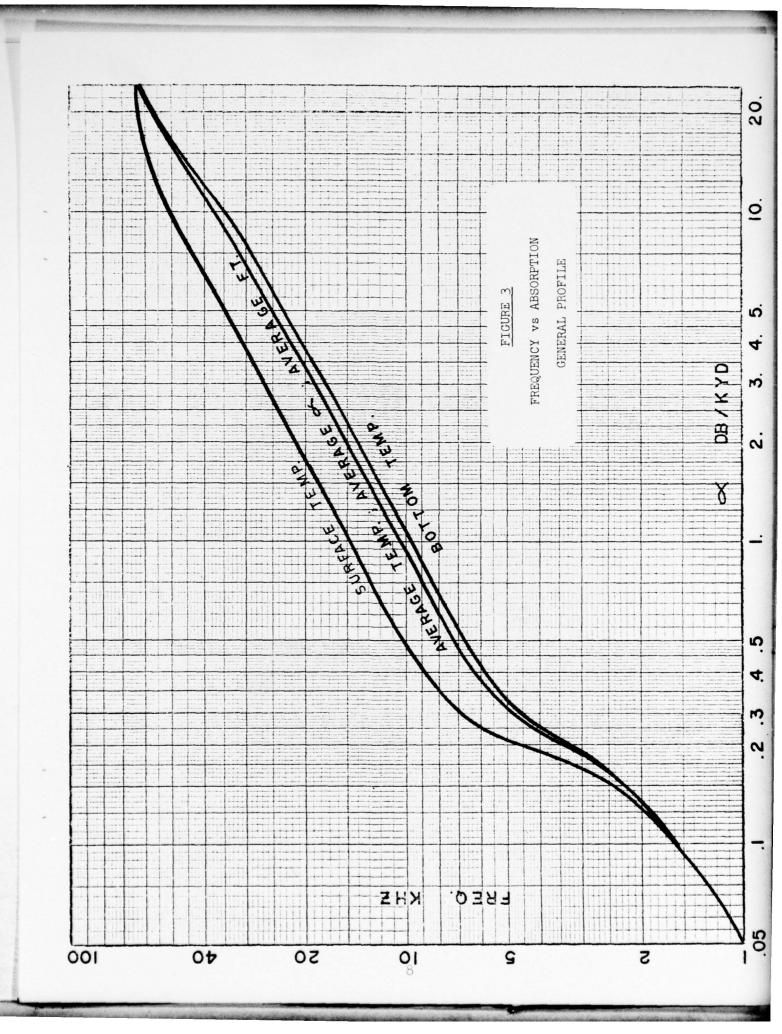
A table is inserted at the end of the report listing the absorption as a function of frequency and temperature for several pressures. Zero pressure is also listed and will coincide with values previously presented. The depth in feet required to produce the pressure is also listed.

## REFERENCES:

- 1. Hall, H. R. and Watson, W. H., "A New Absorption Coefficient Expression for Use in Sonar Range Prediction", U. S. Navy Journal of Underwater Acoustics, CONFIDENTIAL, October 1967.
- 2. Thorp, W. H., "Deep-Ocean Sound Attenuation in the Sub- and Low-Kilocycle-Per-Second Region", Acoustical Society of America Journal, v. 38, p. 648-54, October 1965.
- 3. Marsh, W. H. and Schulkin, M., "Report on the Status of Project AMOS", Research Report No. 255, U. S. Navy Underwater Sound Laboratory, 21 March 1955, CONFIDENTIAL.
- 4. Naval Undersea Warfare Center, Code D556 Internal Report 4, Interim Report on Procedure RAYTRACE, by Dr. H. R. Hall, May 1967.
- 5. Naval Undersea Warfare Center Technical Note 63, Values of the New Acoustic Absorption Coefficient of Seawater, Dr. H. R. Hall, February 1968.



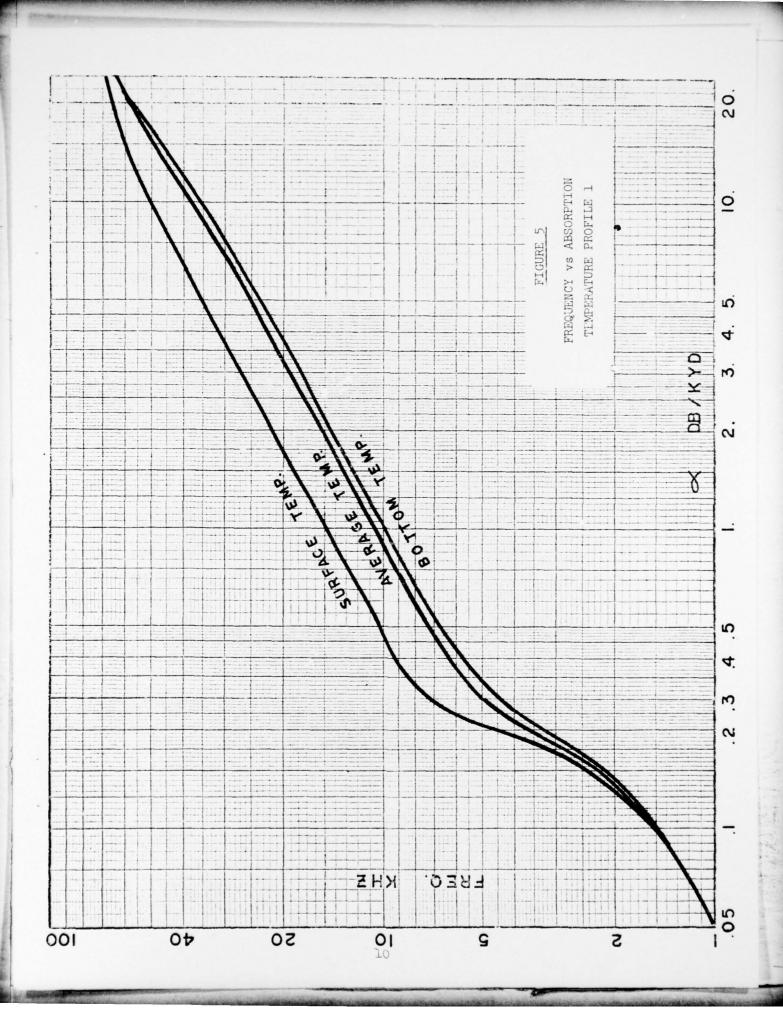


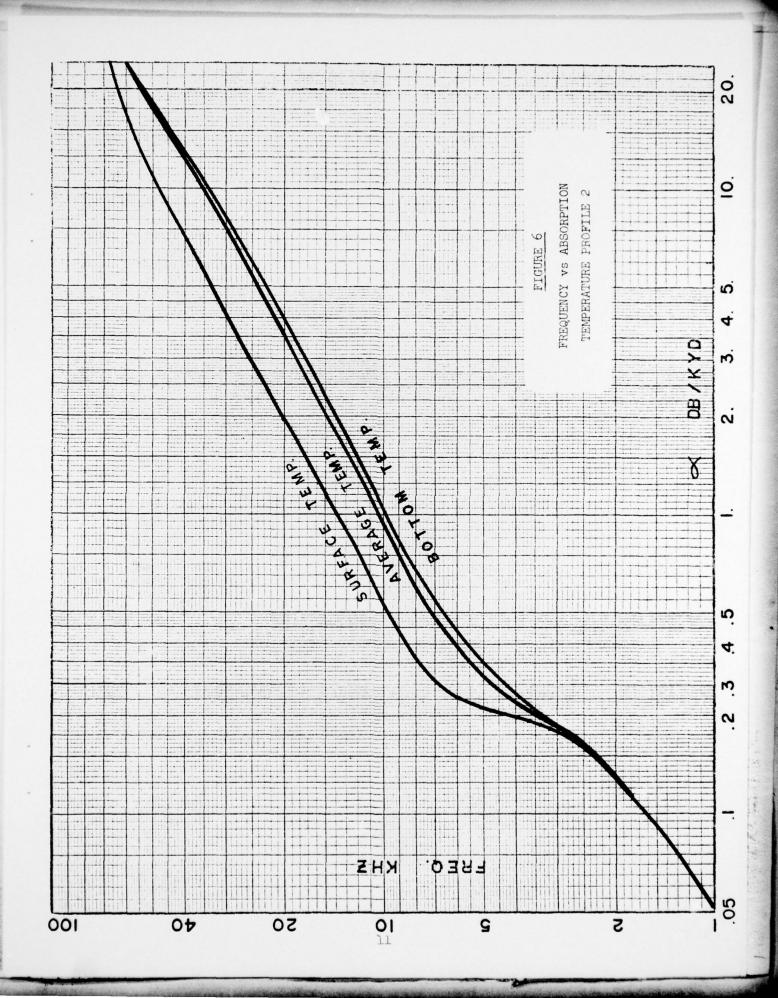


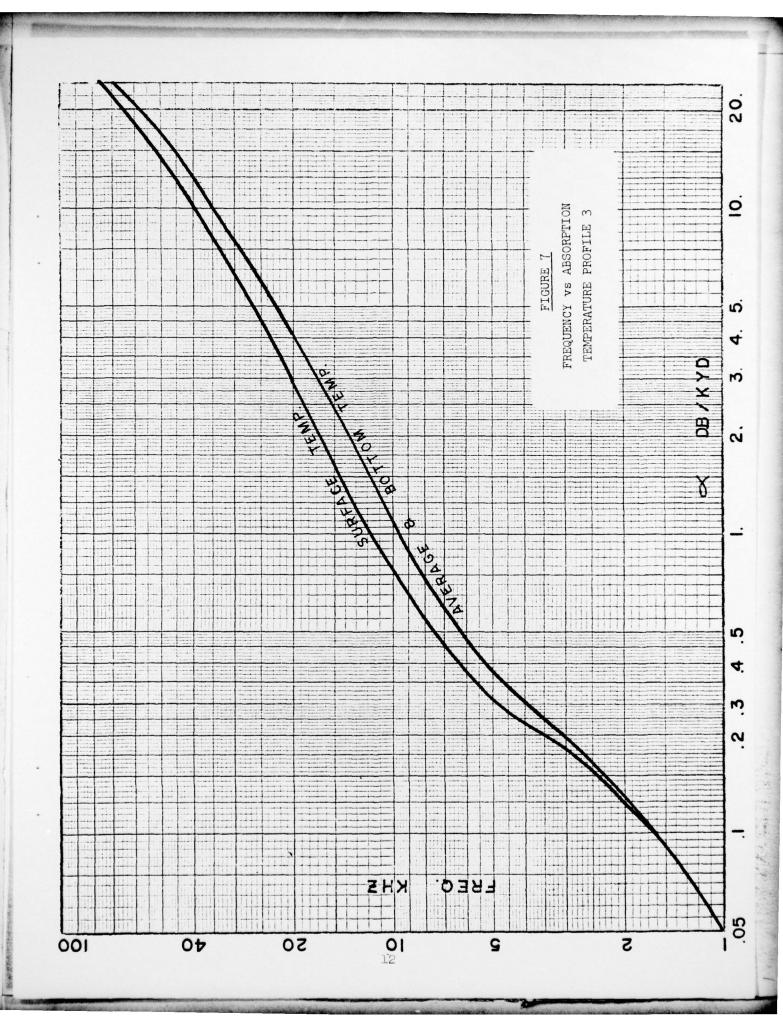
Comparison of the Absorption Loss calculated from the average temperature  $(\overline{T})$  with that calculated from the bottom temperature  $(T_B)$  and the surface temperature  $(T_S)$ .

Frequency khz	$\frac{\left(\alpha(\overline{T}) - \alpha(T_S)\right)_{\times}50}{\text{dB at 50 kyd}}$	$\frac{\left(\alpha(\overline{T}) - \alpha(T_B)\right) \times 50}{\text{dB at 50 kyd}}$
1	.007 dB	002 dB
2	.176	051
3	.91	26
4	2.37	68
5	4.42	-1.27
6	6.95	-1.99
7	9.91	-2.83
8	13.27	-3.78
9	17.03	-4.83
10	21.16	-6.0
20	80.24	-20.8
30	158.8	-36.0
40	236.7	-44.5
50	299.5	-43.3
75	326.4	<b>-7.9</b> 3

Figure Four







FREQUENCY (kHz)	AVERAGE DEPTH (kft)	α (P) (dB/kyd)	α (dB/kyd)	dB DIFFERENCE AT 50 kyd
1	5	0.0527	0.053	0.015
1	10	0.0524	0.053	0.03
1	15	0.0521	0.053	0.045
2	5	0.129	0.13	0.05
2	10	0.128	0.13	0.10
2	15	0.127	0.13	0.15
3	5	0.186	0.19	0.20
3	10	0.182	0.19	0.40
3	15	0.178	0.19	0.61
4	5	0.231	0.24	0.45
4	10	0.222	0.24	0.91
4	15	0.213	0.24	1.36
5	5	0.283	0.30	0.86
5	10	0.267	0.30	1.67
5	15	0.249	0.30	2.58
10	5	0.83	0.91	4.04
10	10	0.751	0.91	8.03
10	15	0.67	0.91	12.12
20	5	3.03	3.36	16.7
20	10	2.71	3.36	32.8
20	15	2.47	3.36	45.

Figure 8. Comparison of  $\,\alpha\,$  calculated with and without pressure term.

TABLES - ABSORPTION COEFFICIENT vs FREQUENCY (kHz) AND TEMPERATURE (°F) FOR VARIOUS PRESSURES (DECIBARS)

PRES	SSURE	.00 DEPTH	LOUIVALENT	0.
		TEMPERA	TURE	
FREQ	25	30	35	40
		5.,		10
2.0	.154001	.132663	.131512	.130520
2.2	.153672	•151448	•149536	.147886
2.5	•172768	•169336	•166383	•163836
2.8	.195212	•189871	•185275	.181309
3.1	.217685	.209928	•203250	•197486
3.5	.248318	.237081	.226970	.218240
1	001510	6.77704	252772	01.5061
4.0	.291519	•273701	.258338	•245054
4.5 5.0	•340156 •395740	•315188 •362700	·293638	.275003
3.0	•393740	• 205100	.334150	.309441
5.h	.472144	.428350	.390451	.357612
6.3	•574689	•517044	•467057	.423678
7.0	•691267	•618501	•555260	•500288
8.0	.860390	.784642	.700603	.627361
9.0	1.096439	.474442	.867604	.774197
10.0	1.356021	1.136588	1.055140	.939820
12.5	2.031055	1.807196	1.607664	1.430855
16.0	3.201485 4.755524	2.867161 4.301529	2.562248 3.873833	2.287292
20.0	4.755524	4.301329	9.07.3733	3.478455
		TEMPERA		
FREO	45	50	55	60
2.0	.129663	•128920	.128275	.127713
2.2	.145461	.145225	.144152	.143217
2.5	.161634	.159726	.158068	.156624
2.8	•177880	•174908	•172325	•170075
3.1 3.5	•192501 •210686	•188179 •2041 <b>3</b> 5	•184422 •198440	•181150 •193477
3.3	•210000	•204133	•190440	•1934//
4.0	.233573	.223603	.214932	.207376
4.5	·258862	.244853	.232664	.222039
5.0	•283024	•269426	•253239	.239125
5.6	•329124	.304369	•282811	.264007
6.3	.356004	• 353237	.324683	.299764
7.0	•452484	•410865	.374571	.342878
8.0	•563534	•507880	•459285	.416811
9.0	•692612	•621345	•559033	•504515
10.0	·838831	• 750443	.673041	.605239
12.5	1.274339	1.137478	1.016649	.910438
16.0	2.041389	1.822657	1.628714	1.457180
20.0	3.113065	2.792759	2.501041	2.240746

		TEMPERA	TURE	
FREQ	65	70	75	80
FKEG	60	70	13	50
2.0	.127222	.126793	.126416	.126085
2.2	.142401	.141687	.141060	.140510
2.5	.155363	.154259	.153291	.152441
2.8	.168110	.166390	•164882	•163557
3.1	•178292	•175791	.173597	.171668
3.5	•189143	•185350	.182022	.179096
4.0	.200775	•194997	.189927	•185470
4.5	•212756	.204629	•197496	•191225
5.0	•226790	.215989	•206509	•198173
5.6	.247507	.233170	.220530	.209415
6.3	•277970	.258875	.242110	.227362
7.0	•315147	290843	•269496	•250716
7.0	•317147	• 290043	•209490	• 230710
8.0	.379521	.347008	.318350	.293129
9.0	.456736	.414813	.377955	• 345505
10.0	•545765	.493544	.447605	.407143
12.5	.817019	.734818	• 562387	•598507
16.0	1.305580	1.171696	1.053377	•948789
20.0	2.009132	1.803473	1.620962	1.459095
		TEMPERA	THRE	
FREG	95	90	95	100
, ,,,,,,,	33			100
2.0	.125793	.125536	.125308	.125106
2.2	.140024	.139596	.139217	.138881
2.5	.151691	.151029	.150444	.149925
2.8	•162388	.161357	.150445	.159636
3.1	•1699bb	•168468	•167141	.165964
2.5	.176518	.174242	.172229	.170444
		4.7207	175007	170004
4.0	.181542	.178074	•175007	.172286
4.5	•185699	•180819	•176502	.172673
5.0	•190826	·184338	•178598	.173507
5.6	.199616	·1909b3	.183307	.176516
6.3	.214360	.202877	.192715	.183702
7.0	.234155	•219527	•206581	.195096
	120.100	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		,,,,,
8.0	.270343	.251228	.233831	.218396
	• 6- 1 1 1 1 1			
9.0	.316873	.291570	.269169	.249292
		The same of the sa	•269169 •311903	.249292 .287094
9.0	•316873 •371426	•291570 •339859	.311903	.287094
9.0 10.0	•316873 •371428 •542067	•291570 •339859 •492136	•311903 •447892	.287094 .408605
9.0	•316873 •371426	•291570 •339859	.311903	.287094

PR_	SSUKE	45.45 DEF	TH EQUIVALENT	1500.
		TEMPS	FATURE	
FRED	25	30		40
2.0	.15300	1 .132382	.131266	.130303
2.2	.15313			.147525
2.5	•17194			.163278
2.8	.19393	.188747	.134283	.180440
3.1	.21532	.208294	.201314	.196222
3.5	•24599	2 .234604	.224793	.216322
4.0	.28721	o •20993(	.255024	.242144
4.5	.33411	2 .309586	.238977	.270896
5.0	.36771	/ •355659		.303984
5.0	.46146	.410974	.382202	.350339
6.3	.56055			.414036
7.0	•67332	•602717	•541356	•488019
8.0	.85599	5 • 753511	.681975	.610905
9.0	1.06571	6 .947347	.843686	.753054
10.0	1.29792	2 1.152931	1.025391	•913500
12.5	1.97135	7 1.754650	1.561050	1.389496
16.0	3.10713	0 2.782749	2.486900	2.220119
20.0	4.61474	o 4.17425	3.759270	3.375645
			ERATURE	
FREO	45	50	55	60
2.0	.12947			.127579
2.2	.14514			.142995
2.5	.10114	2 .159291	•157682	•156280
2.8	.17711			.169539
5.1	•19138			.180371
3.5	•20399	3 .202637	.197111	.192296
4.0	.23099			.205576
4.5	.25523			.219507
5.0	•28320	4 •205150	249453	.235758
5.6	.32259			.259516
6.3	•37748			.293805
7.0	•44163	5 •401254	· 36603A	.335288
8.0	•54337			.406614
9.0	•6/539			.491389
10.0	-81951	3 •729 <b>7</b> 51	•554652	•588864
12.5	1.23 111	9 1.104359		.884550
15.0	1.90152			1.414684
20.0	3.02546	7 2.710327	2.427284	2.174725

PRESS	SURE 4	5.45 DEPT	H EQUIVALENT	1500.
		TEMPER	ATIBE	
EDE:		70	75	80
FREG	55	70	15	nu
2.0	.127103	.126686	.126321	.126000
2.2	.14220		•140902	.140368
2.5	.155057		.153047	.152221
2.5	•13.793	•133700	• 1 300 47	•132221
2.8	.167633	.165965	.164501	.163215
3.1	.177596		.173042	.171171
3.5	.188091	.184410	.181181	.178343
4.0	.199172	•193565	•188646	.184322
4.5	.210499	.202614	.195693	.189609
5.0	.223790	.213310	.204112	.196024
5.6	-243566		.217332	-206547
6.3	.272659		.237864	•223556
7.0	.303381	. 284800	•264088	•245865
8.0	.370529		•311080	.286609
9.0	.445031		• 368591	.337106
10.0	.53115	•480489	•435916	• 396656
12 5	207.20	714140	64.7070	501000
12.5 16.0	.793907		.643872 1.022884	•581890 •921403
20.0	1.207595	the state of the s	1.573366	1.416311
20.0	1.94999	1.750450	1.073300	1.415311
		TEMPER	ATURE	
FREQ	85	90	95	100
2.0	.125717		•125246	.125050
2.2	.139897		.139114	.138788
2.5	.151494	•150852	•150284	.149781
2.8	.162081		•150196	.159411
3.1	.169522	·168066	•166779	•165637
3.5	.175341	.173633	•171679	.169947
			17:160	
4.0	.180510		.174169	.171529
4.5	.184246		•175323	.171608
5.0	.188895	•182600	.177031	.172091
5.6	.197340	.188644	.181215	.174626
6.3	.210940		•189938	.181193
7.0	.229797		.203042	.191899
	•629121	.213003	•203042	•191039
8.0	.265023	.245953	.229074	.214097
9.0	.309325		.263040	.243753
10.0	.362004		.334249	.280176
12.5	.52712	.478681	.435753	.397634
16.0	.831570		•681399	.619652
20.0	1.276926	1.153187	1.043238	.945386
		17		

PRE	SSURE	151.50	DEPT	H EQUIVALENT	5000.
			TEMPERA	ATURE	
FRED	2	25	30	35	40
2.0	.1329		.131727	.130691	.129797
2.2	.151		•149892	.148169	•146683
2.5	.1700	)24	•166931	.164271	•161977
2.8	.1909		.186126	•131985	.178412
3.1	.2114		·204481	.198464	.193272
3.5	.2393	59h	•228823	.219714	.211849
4.0	.2771		.261130	.247290	.235330
4.5	.320		.297517	.278102	.261314
5.0	.3089	999	•339233	.313512	•291251
5.6	.4365		.397099	•362955	.333370
6.3	.5273		• 475653	•430619	.391538
7.0	.6314	143	•565892	•508917	•459392
8.0	.8010	10	.714208	•638500	.572510
9.0	.9940	140	.884129	.737878	.703724
10.0	1.2090	132	1.074406	•955983	.852089
12.5	1.8337		1.632051	1.452291	1.292999
16.0	2.8570		2.585804	2.311104	2.063389
20.0	4.2853	301	3.677293	3.491966	3.135761
			*=un= \		
FRED		. =	TEMPER/	55 55	60
FRES		15	50	.33	50
2.0	.1290	)25	•128355	.127774	.127267
2.2	.1453		.144285	•143318	.142476
2.5	•1599	993	•158274	•156 <b>7</b> 8n	•155479
2.8	.1753		.172645	.170318	.163291
3.1	.1837		.184887	•181503	.178554
3.5	•2050	)44	•199142	.194010	•189540
4.0	.2249		•215996	.208184	.201377
4.5	.246		.234151	•223170	•213598
5.0	.271	357	.255201	•240618	.227902
5.6	.3077	705	.285402	.265980	.249039
6.3	.357		.324077	.302352	.279902
7.0	•4163	324	.378829	•346131	•317578
3.0	•5150		.464868	.421087	.382822
9.0	•6302		•506018	•509881	.460764
10.0	.7511	106	•681476	•611743	•550658
12.5	1.1524		1.028690	•919835	.824146
16.0	1.841		1.544793	1.470064	1.315529
20.0	2.3110	181	2.518005	2.255192	2.020691

PRES	SURE 151.5	DEPTH	EQUIVALENT	5000•
		TEMPERA	THRE	
FREQ	65	70	75	80
, ,,,,,,	,,5			30
2.0	·126825	.125438	•126099	.125801
2.2	.141741	•141097	•140533	•140037
2.5	.154343	•153349	.152477	.151710
2.8	.166520	.164972	.163613	.162418
3.1	.175979	.173726	.171749	.170012
3.5	•1a5635	.182218	.179219	•176584
4.0	.195430	.190225	•185657	.181642
4.5	.205234	197912	.191486	.185937
5.0	.216789	.207059	.198513	.191008
5.6	.234229	.221258	.209870	•199856
0.3	.200267	-243065	•227960	.214674
7.0	.292595	.270699	•251467	•234547
8.0	.349517	.319935	.294116	.271395
9.0	.417719	.379950	.346744	.317509
10.0	•497078	•450030	.408644	.372190
12.5	.739984	•665927	.600673	.543121
16.0	1.178955	1.058329	•951736	.857508
20.0	1.812025	1.626740	1.462313	1.316484
		TEMPERA	TURE	
FREO	85	90	95	100
2.0	.125536	.125306	.125101	.124919
2.2	•139600	.139214	.138973	.138570
2.5	.151035	.150439	.149911	.149444
2.8	.151360	•160437	•159615	.158886
3.1	.168431	•167129	•165933 •170397	•164873
3.5	.174261	•172211	•170397	•168788
4.0	.178105	.174978	.172215	.169763
4.5	•180358	.176401	.172572	.169123
5.0	•184389	.178544	•173373	•163786
5.6	•191020	.183233	.176335	.170217
6.3	.202950	.192614	.183460	.175339
7.0	.219628	.206449	•194785	.184439
5.0	•251352	.233645	.217972	.204066
9.0	.291714	•268918	.248737	.230829
10.0	.340015	.311574	-286388	.264036
12.5	•492374	•447289	•407431	.372036
15.0	.7/4102	.700209	.634660	•576399
20.0	1.187065	1.072170	•970081	.879223
		19		

PRES	SURE 3	03.03 DEPT	H EQUIVALENT	10000.
		TEMPER	ATURE	
FREG	25	30	35	40
2.0	.13186	• 130791	•129869	.123073
2.2	.15011		•146801	.145479
2.5	.10727		•162159	•160117
2.8	.13550	.182379	.178694	.175514
3.1	.20525.		.193678	.189057
3.5	.22997	• 220564	.212457	.205457
4.0	.26234	+ •248557	.236239	•225595
4.5	.29930	.279845	.262564	.247622
5.0	• 34225	• 315762	• 292871	.273058
5.6	.40095	7 • 365842	.335454	.309123
0.3	.40047	.434255	.394175	.359392
7.0	•57161	.513272	•462564	.418487
8.0	.72101		•576379	.517649
9.0	.89162	.793799	.708135	.633240
10.0	1.05202	2 .962204	•856808	.764341
12.5	1.63636		1.296886	1.155117
16.0	2.57240		2.059910	1.839449
20.0	3.81698	2 3.452965	3.110023	2.793003
		TEMPER		
FREG	45	50	55	60
2.0	.12838	.127790	.127273	.126822
2.2	.14433	.143345	.142485	.141735
2.5	•15835	.156822	•155492	.154334
2.8	.17276		.168310	.165506
3.1	.10506		•178582	.175958
3.5	•19940	0 •194148	.189581	.185602
4.0	.21638		.201435	•195376
4.5	.23468		.213674	.205155
5.0	•25538	.240974	.227995	.216678
5.6	·28628		.249146	.234069
6.3	•32918		.230016	.261036
7.0	•30015	7 .346786	•317685	•292274
8.0	.46547		.382882	.343826
9.0	.56782		.460718	.417004
10.0	•65336	6 612495	•550433	•496068
12.5	1.05002		.823000	.737838
16.0	1.64227		1.311386	1.173849
20.0	2.50404	0 2.243202	2.009296	1.800591

, KE 3	3016 303.	os serin	LUGITALL	10000
		TEMPERA		
FREQ	55	70	75	80
2.0	.125428	.126084	.125782	•125517
2.2	.141081	•140508	•140006	.139564
2.5	.153323	•152438	.151662	•150980
2.8	.104931	•153552	•162343	.161280
3.1	.173666	.171661	.169902	•168355
3.5	.102127	•179085	•176417	.174071
4.0	.190084	.185451	•181386	.177812
4.5	.197711	•191195	•185476	.180448
5.0	.205787	.198127	.190526	.183842
5.6	•220330	.209343	.199208	•190296
6.3	.242561	.227251	•213807	.201983
7.0	.270036	•250551	.233434	•218376
8.0	.319006	•292857	•269878	.249656
9.0	.378694	.345079	.315526	.289507
10.0	.448382	•406509	• 369675	.337231
12.5	.662932	•597022	•538946	.487727
20.0	1.052298 1.614378	•944943 1•449974	.850074 1.303633	.766211 1.173847
20.0	1.014370	1.443214	1.000000	1.113041
		TEMPERA		
FREO	35	90	95	100
2.0	.125283	•125077	•124894	.124732
2.2	.139175	•135832	•138528	.138259
2.5	.150379	.149848	•149379	.143963
2.8	.100343	•159516	•158785	.158136
3.1	.106992	•165790	•164726	.163782
3.5	.172004	.170179	•168564	.167133
4.0	.174562	.171882	.169422	.167240
4.5	.176016	.172103	.168642	.165572
5.0	.177951	.172749	•168146	.164064
5.6	.182439	•1/5501	•169362	.163917
6.3 7.0	•191557 •205097	.182350	•174202 •182988	.166975
7.0	1611002	•193368	•108908	.1/5//9
8.0	.251310	.216059	.202110	.189734
9.0	.266550	.246262	.228300	.212362
10.0	·3u3595	•283282	.260867	.241974
10.	11.11.71.71	0.000	144044	7.75.5
12.5	•442472 •691979	•402436 •626214	• 366961 • 567875	•335459 •516024
20.0	1.058662	•956408	• 865547	.784683
20.0	1.03.002	• 750700	• 303 147	• 10.4003

PRESSURE 303.03 DEPTH EQUIVALENT 10000.

PRESS	SURE 454	.50 DEPTH	EQUIVALENT	15000.
		TEMPERA	TURE	
FREQ	25	30	35	40
2.0	.130796	•129855	.129047	•123350
2.2	.148342	.146779	.145435	.144276
2.5	•164535	.162123	.160048	•158258
2.8	.182386	.178634	.175405	.172618
3.1	•199039	•193587	•188894	.184843
3.5	.220556	.212308	.205203	.199067
4.0	.248511	.235989	.225193	.215864
4.5	.279722	.262176	.247032	.233936
5.0	.315519	.292300	.272237	•254872
5.6	.365374	•334598	.307964	•284886
6.3	.433383	• 392872	.357744	• 327259
7.0	.511811	•460675	.416231	•377599
8.0	.641048	.573339	.514284	462810
9.0	.789242	•70350o	.628426	.562782
10.0	•955062	.850047	•757670	.676629
12.5	1.439087	1.281767	1.141544	1.017290
16.0	2.258045	2.023094	1.808821	1.615595
20.0	3.347855	3.028809	2.728237	2.450382
		TE 10501	<b>*&gt;</b>	
(71X17.0)		TEMPERA		
FREQ	45	50	55	60
2.0	.127747	.127225	.126771	.126377
2.2	.143274	.142406	.141651	.140994
2.5	.156711	•155370	.154204	•153189
2.8	.170208	.168119	.156304	.164722
3.1	.181340	•178303	•175663	•173363
3.5	.193759	•189155	•185153	.181665
4.0	.207786	.200782	•194689	.189378
4.5	•222593	•212748	.204181	.196715
5.0	.239822	•226 <b>7</b> 52	•215376	.205457
5.6	.254960	.247469	.232319	.219105
6.3	.300784	.277757	.257690	.240178
7.0	.344005	.314757	•289251	.266979
3.0	.417954	.378843	. 344692	.314844
9.0	•505443	• 455366	•411575	.373262
10.0	•605658	•543543	•489149	•441500
12.5	· 9u7651	.811118	.726205	.651564
16.0	1.442783	1.239066	1.152771	1.032225
20.0	2.197117	1.969503	1.763500	1.580578

PR	ESSURE 454.	50 DEPTH	H EQUIVALENT	15000.
		Tanaaa		
		TEMPERI		
FREQ	65	70	75	80
2.0	.126032	.125730	•125465	.125233
2.2	.140421	.139919	.139479	.139092
2.5	.152303	.151528	•150847	•150250
2.8	.103342	.162133	.161073	.160142
3.1	.171355	.169597	•168055	.166699
3.5	.178619	•175954	•173615	.171559
4.0	.184740	.180679	•177116	.173984
4.5	.190191	.184479	.179467	.175060
5.0	.196789	•139198	•192536	.176678
5.6	•207552	.197434	.188551	.180740
6.3	.224362	.211443	.199661	.189297
7.0	.247490	.230411	•215409	.202211
8.0	.288708	•265790	.245650	.227926
9.0	•339685	.310224	.284321	.261517
10.0	.399704	.363005	•330721	.302286
12.5		•528146	.477245	.432353
16.0		.831601	.748451	.674950
20.0	1.417810	1.273279	1.145020	1.031265
		TEMPER.	And the second s	
FREG	35	90	95	100
2.0	.125028	.124847	.124687	.124545
2.2		.138450	.138184	.137948
2.5	.149723	•149258	•148846	•148482
2.8	.159321	.158596	.157955	.157387
3.1		.164451	.163518	.162691
3.5	•109747	•168148	•166733	•165478
4.0		.163787	.166631	.164718
4.5		.167747	.164713	.162022
5.0	•171515	•166955	.162922	.159344
5.6		•167773	.162392	.157620
6.3		•172090	.164949	.159514
7.0	•190573	•180293	.171195	.163124
8.0		.198480	.186254	.175407
9.0		.223614	.207872	.193902
10.0	•277188	·2550u2	.235357	.217921
12.5		.357599	.326507	.299898
16.0		.552249	.501118	•455673
20.0	.930314	.840691	.761056	.690183